

Assumptions

* no intermediary P-ATG-LacS_2 complex

stochastic effects // Binding of LacS to ATG can be more complex
we assume 2 LacS for 1 $\text{ATG} \dots$

II Before ATG is introduced ...

$$\begin{cases} \frac{d[\text{ATG}]}{dt} = k_3 [\text{P}] - k_2 [\text{ATG}] \\ \frac{d[\text{LacS}]}{dt} = k_1 - d_1 [\text{LacS}] + k_5 [\text{P-LacS}_2] - k_4 [\text{P}] [\text{LacS}]^2 \\ \frac{d[\text{P}]}{dt} = -k_4 [\text{P}] [\text{LacS}]^2 + k_5 [\text{P-LacS}_2] \\ \quad = -\frac{d[\text{P-LacS}_2]}{dt} \end{cases}$$

ATG introduced @ steady state of previous system

$$[\text{LacS}] = k_1 / d_1$$

$$[\text{P-LacS}_2] = K_P [\text{P}] [\text{LacS}]^2$$

conservation of monomers $P_0 = \text{P} + [\text{P-LacS}_2]$

$$\text{P} = \frac{P_0}{1 + K_P [\text{LacS}]^2}$$

$$[\text{P-LacS}_2] = \frac{K_P [\text{LacS}]^2}{1 + K_P [\text{LacS}]^2}$$

$$[\text{ATG}]_{ss} = \frac{k_3 P_0}{(1 + K_P [\text{LacS}]^2) \times d_1 \text{ATG}}$$

basal rate concentration

1

III

steady state expression of LacI unbinding of bound LacI Binding of free LacI

$$\frac{d[LacI]}{dt} = k_1 - d_1 [LacI] + k_5 [P - lacI_2] - k_4 [P] [LacI]^2 - k_2 [IPTG] [LacI]^2 + k_3 [IPTG - lacI_2]$$

Binding of free LacI Unbinding of bound LacI

$$\frac{d[IPTG]}{dt} = -k_2 [IPTG] [LacI]^2 + k_3 [IPTG - lacI_2] - k_6 [IPTG] [P - lacI_2] + k_7 [P] [IPTG - lacI_2]$$

Binding of free IPTG Unbinding of bound IPTG

LacI-IPTG complex

$$\frac{d[IPTG - lacI_2]}{dt} = k_2 [LacI]^2 [IPTG] - k_3 [IPTG - lacI_2] + k_6 [IPTG] [P - lacI_2] - k_7 [P] [IPTG - lacI_2]$$

Complex formation Complex dissociation

P = free promoter

$$\frac{d[P]}{dt} = -k_4 [P] [LacI]^2 + k_5 [P - lacI_2] + k_6 [IPTG] [P - lacI_2] - k_7 [P] [IPTG - lacI_2]$$

Complex dissociation Complex formation Complex dissociation

P-lacI = promoter-lacI complex

$$\frac{d[P - lacI_2]}{dt} = +k_4 [P] [LacI]^2 - k_5 [P - lacI_2] - k_6 [IPTG] [P - lacI_2] + k_7 [P] [IPTG - lacI_2]$$

Complex formation Complex dissociation Complex dissociation

a) steady state all $\frac{d}{dt} = 0$

$$\begin{aligned} [LacI]_s &= k_1 / d_1 \\ [IPTG - lacI_2] &= k_2 [LacI]_s^2 [IPTG] \\ [P - lacI_2] &= k_4 [P] [LacI]_s^2 \\ [P] [IPTG - lacI_2] &= k_5 [P - lacI_2] \end{aligned}$$

$$\begin{aligned} P_0 &= P + [P - lacI_2] \\ I_0 &= [IPTG] + [IPTG - lacI_2] \end{aligned}$$

⇒ Problems!!

Let equation (*) not apply

⇒ we need complex P-IPTG-lacI!!

IV Looking for the Steady States: $\frac{d}{dt}$ of everything $\Rightarrow 0$.

Temporary Notations:

$$A = k_2 [IPTG][lacI]^2 - k_3 [IPTG-lacI_2]$$

$$B = k_4 [P][lacI]^2 - k_5 [P-lacI_2]$$

$$C = k_6 [IPTG][P-lacI_2] - k_7 [P][IPTG-lacI_2]$$

* @ steady states we have

$$\left. \begin{aligned} A + C = 0 & \text{ from } d[IPTG]/dt = 0. \\ B - C = 0 & \text{ from } dP/dt = 0. \end{aligned} \right\} \Rightarrow \begin{aligned} A + C + B - C &= 0 + 0 \Rightarrow A + B = 0. \\ \Rightarrow [lacI] &= k_1/d. \end{aligned}$$

$$k_1 - d_1 [lacI] - B - A = 0 \text{ from } d[lacI]/dt = 0.$$

* Conservation Equations

$$P_0 = [P] + [P-lacI_2]$$

Conservation of promoter

$$I_0 = \frac{[IPTG]}{I} + [IPTG-lacI_2]$$

Conservation of IPTG.

$$A + B = k_2 [lacI]^2 [IPTG] - k_3 (I_0 - I) + k_4 [P][lacI]^2 - k_5 (P_0 - P) = 0$$

← from conservation equation

← from conservation equation.

Rearranging the above:

$$\boxed{[k_2 [lacI]^2 + k_3] I} + (k_4 [lacI]^2 + k_5) P = k_3 I_0 + k_5 P_0$$

Notation: $\alpha = [lacI]_{ss}^2$

** Notation $\alpha = [lacI]_{ss}^2$

$$(1) \quad \alpha I + (k_4 \alpha + k_5) P = k_3 I_0 + k_5 P_0$$

↙ Rewriting in a similar manner!

$$A + C = k_2 \alpha I - k_3 (I_0 - I) + k_6 I (P_0 - P) - k_7 P (I_0 - I) = 0$$

$$\Rightarrow (2) \quad (\alpha k_2 + k_3 + k_6 P_0) I - k_7 I_0 P + (k_7 - k_6) I P = k_3 I_0$$

how has he substituted $(\alpha k_2 + k_3) I$ for I ?

$$\boxed{(\alpha k_2 + k_3) I} = k_3 I_0 + k_5 P_0 - (k_4 \alpha + k_5) P$$

Solve simultaneously.

and put the $(\alpha k_2 + k_3)$ here.

Substitute I into (2) \Rightarrow

$$(\alpha k_2 + k_3 + k_6 P_0) (k_3 I_0 + k_5 P_0 - (k_4 \alpha + k_5) P) - k_7 I_0 (\alpha k_2 + k_3) P + (k_7 - k_6) P (k_3 I_0 + k_5 P_0 - (k_4 \alpha + k_5) P) = k_3 I_0 (\alpha k_2 + k_3)$$

$$(3) \quad + (k_7 - k_6) P (k_3 I_0 + k_5 P_0 - (k_4 \alpha + k_5) P) = k_3 I_0 (\alpha k_2 + k_3)$$

And Divide by $(\alpha k_2 + k_3)$ and multiply through

and therefore Rewriting terms in P^2

terms in P

$$P^2 (k_6 - k_7) (ak_1 + k_5) - P ((ak_1 k_5) (ak_2 + k_3 + k_6 P_0) + k_7 I_0 (ak_2 + k_3) + (k_6 - k_7) (k_3 I_0 + k_5 P_0)) + k_7 I_0 (ak_2 + k_3) = 0$$

which can be rewritten as How?.

$$P^2 (k_6 - k_7) (ak_1 + k_5) - P ((ak_1 k_5) (ak_2 + k_3 + k_6 P_0) + k_7 I_0 (ak_2 + k_3) + (k_6 - k_7) (k_3 I_0 + k_5 P_0)) + k_7 I_0 (P_\infty - P) \times (k_3 k_6 + ak_2 k_7) = 0 \quad || \quad P_0$$

what does this represent? P at $I = \infty$
 $\frac{P_0 \text{ Bound}}{1 + a k_1 k_5 / k_6}$
 as a proportion of all.

~~$P_\infty = \dots$~~ $P_\infty \sim P_0$
 Initial condition $P = \frac{P_0}{1 + a k_1 k_5 / k_6}$
 initial promotes \rightarrow \leftarrow Bound promotes

This suggests that we solve with $X = P/P_0$
 $X =$ preparation of promoters that will express GFP

The equation can be rewritten as

$$X^2 (k_6 - k_7) (ak_1 + k_5) - X (k_5 (k_6 - k_7) + (ak_1 + k_5) \frac{(ak_2 + k_3 + k_6 P_0)}{P_0}) + k_5 \left(\frac{ak_2 + k_3 + k_6 P_0}{P_0} + k_6 \right) + I_0 (X_\infty - X) \frac{k_3 k_6 + ak_2 k_7}{P_0} = 0$$

How have we gotten this P^2 to $= P^2 / P_0^2$

notation $b = \frac{ak_2 + k_3 + k_6 P_0}{P_0} + k_6$

$$Q(X) = (k_6 - k_7) (ak_1 + k_5) \left\{ X^2 - X \left[\frac{k_5}{ak_1 + k_5} + \frac{b}{k_6 - k_7} \right] + \frac{k_5}{ak_1 + k_5} \times \frac{b}{k_6 - k_7} \right\}$$

roots of $Q = \frac{k_5}{ak_1 + k_5} = \frac{1}{ak_1 P + 1}$
 corresponds to $I_0 = 1$

4b.)

$$C = \frac{K_2 K_0 + a K_2 K_7}{P_0 (K_0 - K_7) (a K_2 + K_5)} = \frac{K_3 (K_8 + a K_9)}{P_0 (K_8 - 1) (a K_2 + K_5)}$$

$$R(X) = C (X_\infty - X)$$

V And Now for the solutions

* The easy part

Q(x) has at least one positive solution

$$X_1 = \frac{1}{a k_{p+1}} \quad (\text{the steady state if } I_0 = 0)$$

$$X_2 = \frac{b}{k_6 - k_7} \quad \text{is also acceptable if } k_8 \gg 1$$

R(x) has only one root X_∞

as $I_0 \rightarrow \infty$ ~~Q(x) \neq I_0 R(x)~~ degenerates

~~into~~ $I_0 R(x) \approx Q(x) + I_0 R(x)$ increases
the weight of

In particular the roots (complex or not) converge to X_∞

** First Case $k_6 \ll k_7$ ($c < 0$)

Q(x) has only one root that is positive

For $I_0 > 0$, we seek the roots of

$$(X - X_1)(X - X_2) + c I_0 (X_\infty - X) = 0$$

To make the calculation easier we let

$$Y = X - X_1 \quad Y_2 = X_2 - X_1 (< 0) \quad Y_\infty = X_\infty - X_1$$

$$Y(Y - Y_2) + c I_0 (Y_\infty - Y) = 0$$

$$-Y^2 - Y(Y_2 + c I_0) + c I_0 Y_\infty = 0$$

$$Y = \frac{Y_2 + c I_0 \pm \sqrt{(Y_2 + c I_0)^2 - 4c I_0 Y_\infty}}{2}$$

(+) for I_0 close to zero

~~***~~ $K_0 < K_1$ and $X_0 > X_1$, the nice case (6)

$X_0 > 0 \rightarrow$ discriminant equation always > 0

$$Y = \frac{Y_2 + cI_0 + \sqrt{(Y_2 + cI_0)^2 - 4cI_0X_0}}{2}$$

Evolution of the solution

$$2 \frac{dY}{dI_0} = c + \frac{1}{2\sqrt{\dots}} (-4cX_0 + 2c(Y_2 + cI_0))$$

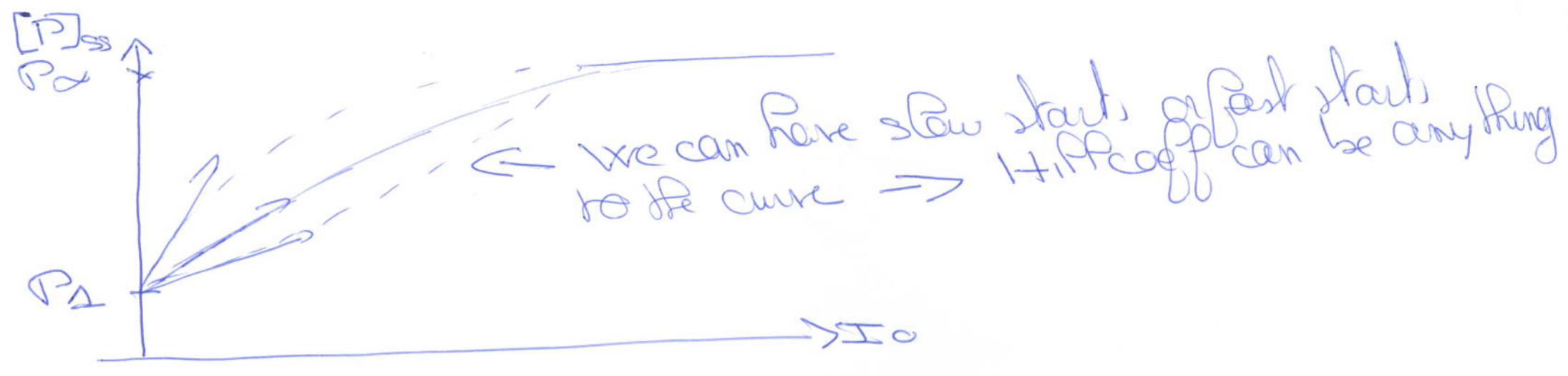
$$= \frac{c}{\sqrt{\dots}} (\sqrt{\dots} - 2X_0 + Y_2 + cI_0)$$

@ $I_0 = 0 \quad \frac{dY}{dI_0} = \frac{-2cX_0}{|Y_2|} > 0$

sign $\frac{dY}{dI_0} = -\text{sign} \left(\frac{\sqrt{\dots} - 2X_0 + Y_2 + cI_0}{< 0} \right)$

$$= -\text{sign} \left((Y_2 + cI_0)^2 - 4cI_0X_0 \right) = (Y_2 + cI_0 - 2X_0)^2$$

$$= -\text{sign} \left(-4cI_0X_0 - 4X_0^2 + 4X_0(Y_2 + cI_0) \right) > 0$$



~~***~~ Complement: what does $X_0 > X_1$ mean?

it means $K_B > K_A | K_D$

K_B : allocation rate of the 'repression' (Bop)

$\text{Loc } I \rightarrow \text{Loc } I_2 \neq P$ (direct bunding)

When IOTG is introduced, another way to repress is

enabled: the 'backward way'

$\text{Loc } I \rightarrow \text{IOTG} - \text{Loc } I_2 \rightarrow \text{Loc } I_2 - P$

The dissociation constant of the other route is K_{α}/K_{β}

If this route is more attractive than the direct route

($K_{\alpha}/K_{\beta} > K_{\alpha}$), we require even more \Rightarrow

$$\text{as } [G_{\alpha\beta}] < [G_{\alpha}]_{\beta=0}$$

If on the contrary, the backward route is less attractive, adding this route will favour repression $\Rightarrow [G_{\alpha\beta}]_{\beta=0} > \dots$

$$*** \quad x_0 < x_1 \quad \& \quad x_2 < x_1$$

7

The discriminant of the equation is

$$\Delta = (\gamma_2 + c\Gamma_0)^2 - 4c\Gamma_0\gamma_2$$

that is

$$\Delta = \cancel{x}^2 + x(2\gamma_2 - 4\gamma_2) + \gamma_2^2 \quad x = c\Gamma_0$$

we have a solution iff $\Delta \geq 0$

$\Delta(x)$ poly in x

For $x > 0$, $\Delta(x) \geq 0$ iff $2\gamma_2 - 4\gamma_2 \leq 0$ i.e. $\gamma_2 \leq 2\gamma_2$
(both possible roots ≤ 0)

$$\text{or } \Delta = (2\gamma_2 - 4\gamma_2)^2 - 4\gamma_2^2 < 0$$

(no real solutions)

$$\text{i.e. } -16\gamma_2\gamma_2 + 16\gamma_2^2 < 0$$

$$\gamma_2^2 (\gamma_2 - \gamma_2) < 0$$

$$\text{i.e. } \gamma_2 \geq \gamma_2$$

$$\| \Delta(x) \geq 0 \text{ iff } \gamma_2 \leq 2\gamma_2$$

Then we have $\gamma(\Gamma_0) \downarrow \beta^n$ of \mathcal{F}_0

iff $0 > \gamma_2 > \gamma_2$, then for $\mathcal{F}_0 > \mathcal{F}_0$ next,
there are no real steady points !!

But it is impossible $x_2 < 0$; $x_2 > 0$

$$\Rightarrow \gamma_2 < \gamma_2$$

Proof

⑧ Second Case $k_0 > k_1$ $c > 0$

Q(x) has 2 real, positive solutions

* First important result: for $k_0 > k_1$ $x_2 > x_1$ and $x_2 > x_\infty$

proof $b = k_0 + \frac{a k_0 k_1}{\rho_0} > k_0$

$$\Rightarrow \frac{b}{k_0 - k_1} > 1$$

and $x_1 = \frac{1}{1 + a k_1} < 1$ (same for x_∞)

Good News: ~~There are~~ fewer cases to study,

* First Possibility $x_\infty < x_1$ i.e. $x_\infty < 0$

∴ before we now seek the roots of

$$Y(Y - Y_2) + c I_0 (Y_\infty - Y) = 0$$

$$\text{that is } Y^2 - Y(Y_2 + c I_0 Y_\infty) + \frac{c I_0 Y_\infty}{c_0} = 0$$

2 roots of opposite signs

∴ the root we are interested in is

$$Y = \frac{Y_2 + c I_0 Y_\infty - \sqrt{(Y_2 + c I_0 Y_\infty)^2 - 4 c I_0 Y_\infty}}{2} < 0$$

$Y(I_0)$ decreasing function $\begin{cases} Y(0) = Y_1 = 0 \\ Y(+\infty) = Y_\infty \end{cases}$

* * Other Possibility $x_\infty > 0$

The discriminant of the equation is

$$(Y_2 + c I_0 Y_\infty)^2 - 4 c I_0 Y_\infty > (Y_\infty + c I_0 Y_\infty)^2 - 4 c I_0 Y_\infty > 0$$

no problem

$$Y(I_0) = \frac{Y_2 + c I_0 Y_\infty - \sqrt{(Y_2 + c I_0 Y_\infty)^2 - 4 c I_0 Y_\infty}}{2}$$

growing function of I_0

VII Final Thought...

• Simulations confirm the results obtained in this analysis

* Influence of degradation terms non negligible.

- if d_1 large enough, $P(t)$ is not monotonous



- Therefore if d_1 is large enough, $G(t)$ also exhibits a bump!!

- degradation terms, ~~not~~ in practice will likely be small \Rightarrow my prediction is no bump!

* $K_{\text{loss}} = K_{\alpha} / K_{\gamma}$ and K_{ρ} determine the dynamics of the construct

The gain $K_{\rho} / K_{\text{loss}}$ is, the gain the gain in fluorescence

* $[G(t)]_{ss}$ (I_0) can be approximated by a Hill function in practice. (at least an offset!) \rightarrow

* Ideal Construct

$$\left(\begin{array}{l} K_{\rho} (k_1/d_1)^2 \text{ large} \\ (K_{\alpha}/K_{\gamma}) \cdot (k_1/d_1)^2 \text{ low} \end{array} \right)$$

\rightarrow we want K_{ρ} large
 K_{α}/K_{γ} low
a ~~small~~ large.

\Rightarrow Constitutive promoter: as strong as possible
and of course K_{γ} as large as possible